

Recy procedures

Calculate

$h(x,y)$ = computed heads

$q_s(h)$ = computed baseflow

P = pumping

Calculate state impacts $\Delta Q \approx \left(\frac{\partial q}{\partial P} \right) \Delta P$

If stream is dry w/ all-on condition:

start with all-off condition. if stream $\neq 0$ with all-off, depletion is zero + we're done. otherwise use bisection

to determine fraction of pumping that uses all streamflow, and remainder comes from storage. For that fraction of pumping

F_P that uses all streamflow, calculate each state's contribution

If $q_s > 0$ with all on, then ~~similarity~~ assume known h

$$\Delta Q = \begin{matrix} Q_{all\ on, q_s} - Q_{all\ on, P_{on}} \\ \vdots \\ Q_{all\ off, P_{off}} - Q_{all\ off, P_{on}} \\ \vdots \end{matrix}$$

ΔQ should be $\approx \sum \Delta Q_i$

else

find fraction F of all pumping at which stream goes dry

then calculate total + compared depletions to before

but total in condition P_{off} and $F P_{on}$ where:

$$\Delta Q = Q|_{P_{off}} - Q|_{F P_{on}}$$

$$\Delta Q_c = Q|_{P_{off}} - Q|_{all\ F P_{on}}$$

test procedure for 2003

1. Calculate Run Model determine f

Run model for all f for $f_k = 0, .2, .4, .6, .8, 1$
 for each impact can calc h_i for some f values
 reach a time step

for each [account]: find f_k at which storage is
 completely depleted. then for each (impact run)
 calculate component depletions

2003:

total impact

| | | | | | | | | | | | |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| ϕ | ϕ | ϕ | ϕ | ϕ | ϕ | ϕ | ϕ | ϕ | ϕ | ϕ | ϕ |
| 0 | .1 | .2 | .3 | .4 | .5 | .6 | .7 | .8 | .9 | 1 | |

h_i 0 .1 .25 .5 .75 .9 1

| | | | | | | | |
|----------------------|---|----|----|----|----|---|----------------------|
| $f_{k, i=1,2,3,4}$ | 0 | .2 | .4 | .6 | .8 | 1 | $k = 0, 1, \dots, 5$ |
| each state $f_{k,i}$ | 0 | .2 | .4 | .6 | .8 | | |

$i=1,2,3,4$

$f_{k,i} = 0$ corresponds to NO PUMP (or) a MOUND condition.

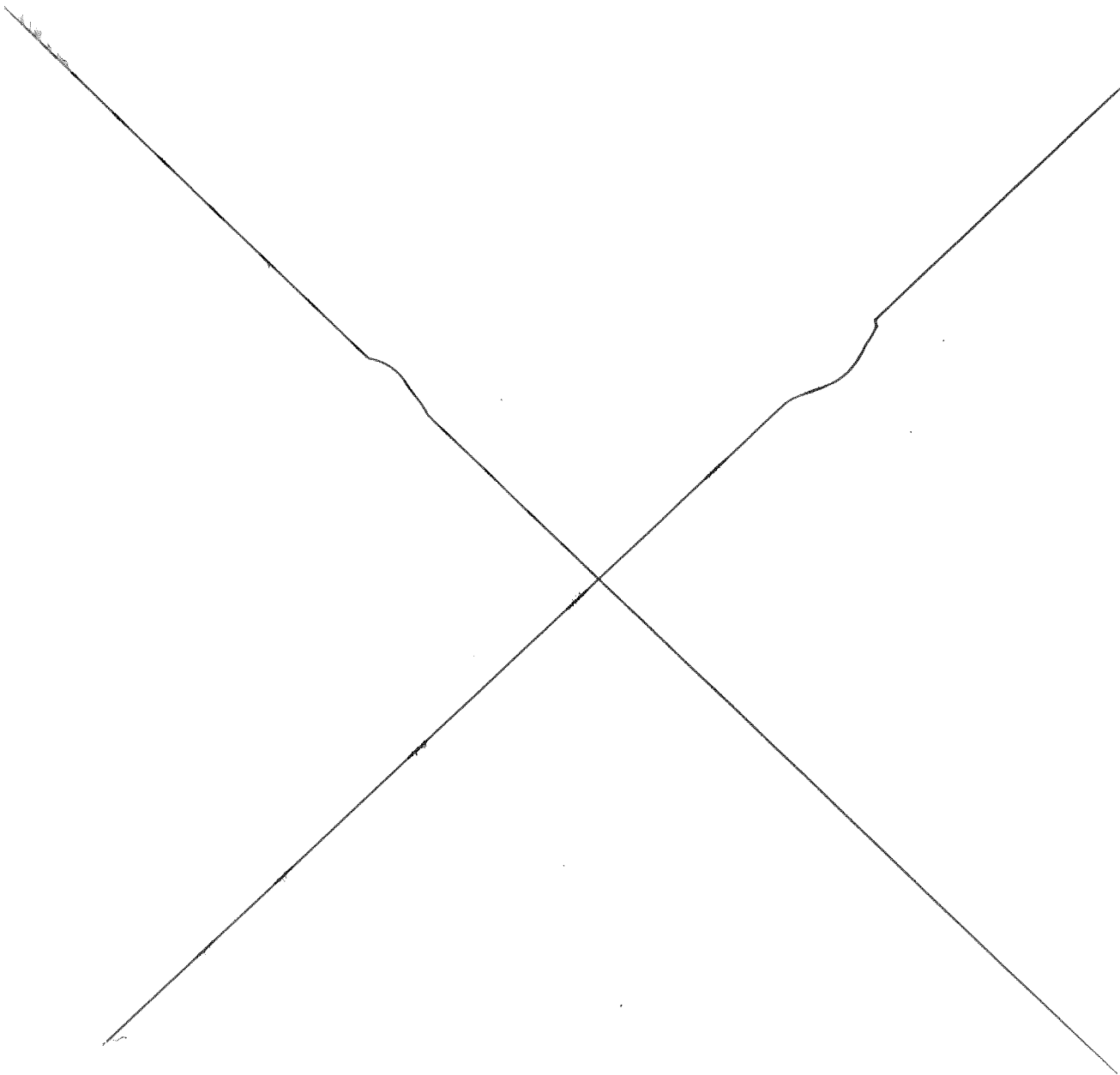
$$\Delta Q = Q_{OFF} - Q_k$$

$$SD_i = Q_{oi} - Q_{ki} \text{ for pumping from } k \text{ and impact case } i.$$

From WWS case: $\Delta \sigma_{ijk}$ for $k=1$

From base case: back off each stress by SF.
From σ for each orientation of total pumping P

For compare to base case (with P total pumping P)



~~base 12p_test.d.nam 12p_test.rch, n.wel, n.out, n.5fi
all off 12p.0_all.nam~~

LSX 2011

pumping impacts Test 4 1918-2010.xls

2:20 pm 4/3/2012

- created in c:\gw\rrca\bn2001\impacts base (laptop)
copied to L:\app\rrca\2012\all_acc\revise
and to c:\gw\rrca\bn2001\impacts base

$$\begin{aligned} \mathcal{E} &\approx T_h + \frac{1}{3} (T_h - T_{2h}) && \text{for } q=2, p=2 \\ &= \frac{1}{3} (4T_h - T_{2h}) && \text{eqn 7.2.12} \end{aligned}$$

Dahlquist + Björk p. 271
 Conte & de Boor p. 339
 Press et al. p. 113 eq. 4.2.9

for $q=2, p=1$ $A_{m,k} = A_{m,k-1} + (A_{m,k-1} - A_{m-1,k-1})$
 error is $O(h)$

For $q=2.5, p=1$ $A = A$

$$\begin{aligned} F(0) &= F(h) + \frac{F(h) - f(qh)}{q^p - 1} \\ &= F(0.2) + \frac{F(0.2) - f(0.5)}{2.5 - 1} = \frac{f(0.2) - f(0.5)}{1.5} \\ &= f(0.2) \left(1 + \frac{1}{1.5} \right) - \frac{f(0.5)}{1.5} \\ &= f(0.2) \left(\frac{2.5}{1.5} \right) - \frac{f(0.5)}{1.5} \\ &= \frac{1}{1.5} (2.5 f(0.2) - f(0.5)) \end{aligned}$$

if $|e(h)| < 0.5$

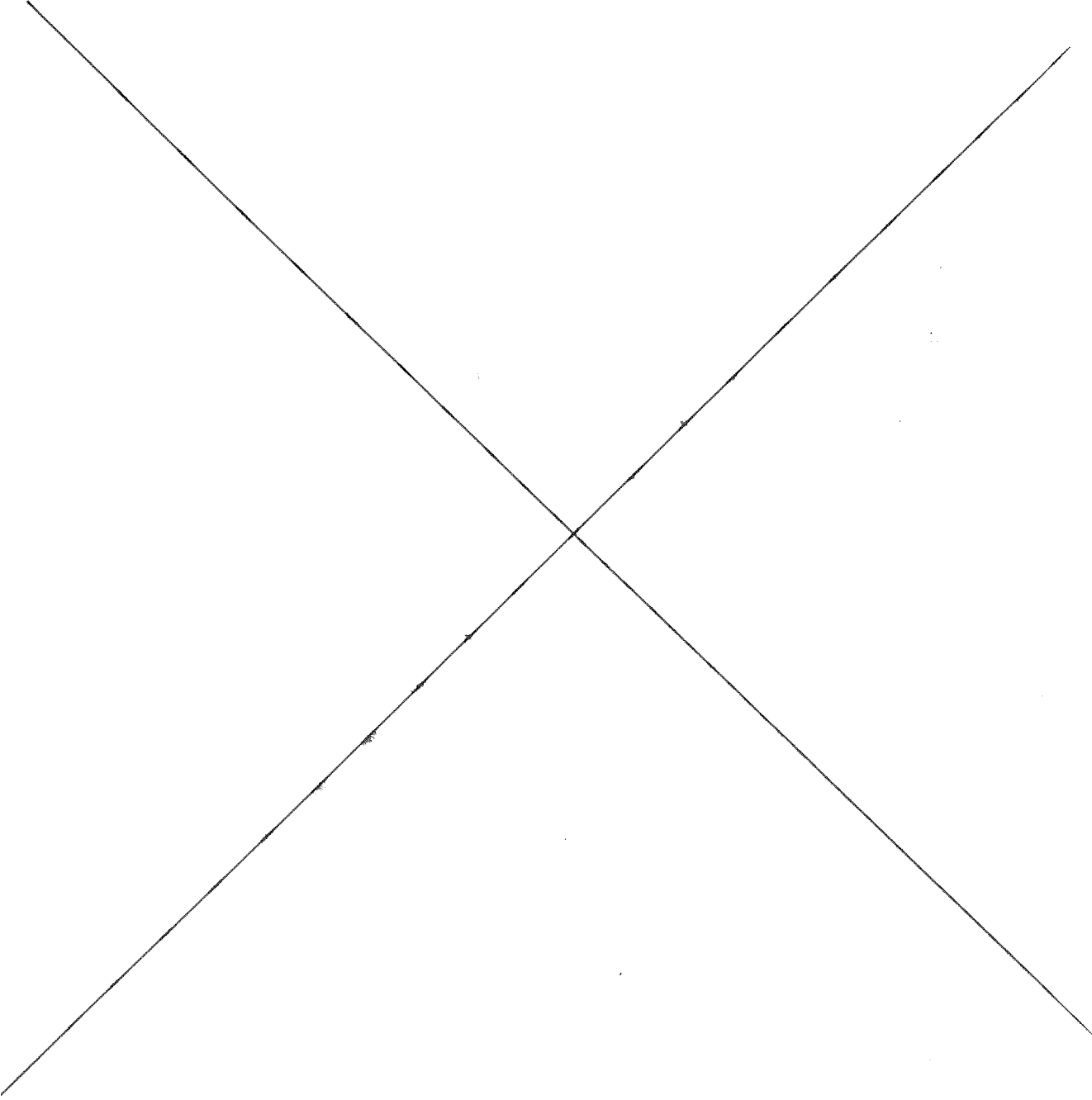
then $A(0) \approx A(h)$

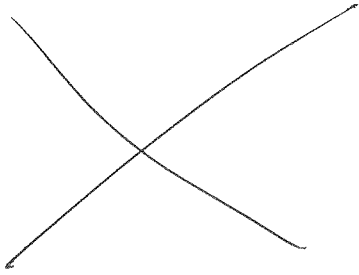
if $(\text{abs } A - |A$

else if $|e(h)| > |e(qh)|$ then \square

then $A(0) \approx A(qh)$

else $A(0) = A(h) + (A(h) - A(qh)) / (q^p - 1)$





Thursday
May 10, 2012

run_pta_to_1_pt2_incr.bat

args: 1 2 3 4

call incr_stress_v2 0 0.2 0 2

sub_incr_stress_v2 %1 %2 %3 %4

call sub_ptx %2 %1 %1 %1 %3 -pt%4 CO

0.2 0 0 0 0 -pt+2CO

| | co | KS | NE | MD | | co | KS | NE | MD | co | KS | NE | MD |
|------------|----|----|----|----|--------|-----|-----|-----|-----|-----|-----|-----|-----|
| all on | 1 | 1 | 1 | 1 | base | 1 | 1 | 1 | 1 | 0 | 0 | 0 | 0 |
| all off | 0 | 0 | 0 | 0 | z/base | 0.9 | 0.9 | 0.9 | 0.9 | 0.1 | 0.1 | 0.1 | 0.1 |
| CKN PMP ON | 1 | 1 | 1 | 0 | d/base | 1 | 1 | 1 | 0.9 | 0.1 | 0 | 0 | 0 |
| KN COMBOFF | 0 | 1 | 1 | 0 | ad/d | 0.9 | 1 | 1 | 0.9 | | | | |
| CN KSMDOFF | 1 | 0 | 1 | 0 | bd/d | 1 | 0.9 | 1 | 0 | | | | |
| CK NEMDOFF | 1 | 1 | 0 | 0 | cd/d | 1 | 1 | 0.9 | 0 | | | | |

Impact sum: $(ad - d) + (bd - d) + (cd - d) + (d - base)$
z-base: $(ad - d) + (bd - d) + (cd - base)$

1/scr

[2]

| | co | KS | NE | MD | | | | | |
|---------|-----|-----|-----|-----|--|-----|-----|-----|-----|
| base | 1 | 1 | 1 | 0 | | 0 | 0 | 0 | 0 |
| all off | 0.9 | 0.9 | 0.9 | 0.9 | | 0.1 | 0 | 0 | 0 |
| MD | 1 | 1 | 1 | 1 | | | | | |
| d | 1 | 1 | 1 | 0 | | 0 | 0 | 0 | 0 |
| ad/d | 0.9 | 1 | 1 | 0 | | 0.1 | 0 | 0 | 0 |
| bd/d | 1 | 0.9 | 1 | 0 | | 0 | 0.1 | 0 | 0 |
| cd/d | 1 | 1 | 0.9 | 0 | | 0 | 0 | 0.1 | 0 |
| base MD | 1 | 1 | 1 | 1 | | 0 | 0 | 0 | 0.1 |
| | | | | | | 0.1 | 0.1 | 0.1 | 0.1 |